

7. V annumber updates sin to to an adde to an annumperature of the state of the state of the billing way and the state of the state of the state way with a data pairs againstate oversite rate angle state way and hereases to be state of the state angle of the state of hereases the state of the state angle of the state of hereases the state of the state angle of the state of hereases and the state of the hereases the state of the state of the state of the hereases the state of the state of the state of the hereases the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the state of the state of the state of the hereases the state of the hereases the state of the

impedance is around 5 k . Sinking too much of current from

Although differential input rejects commomode noise inherently,the commorimode voltage on each of the input pin still affects the operation of the controller. A commonimode filter is generally implemented to filter out the commorimode noise. Figure 11. shows a schematic of the commorimode filter. Bandwidth of the commorimode filteris

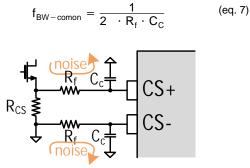


Figure 11. Common ïmode Filter for CS Pin

Due to a mismatch between the resistors and capacitors in the commorimode filter, commorimode noise may be filtered differently between CS+ and CSAs a result, a differentialimode noise appears **dhe** CS signals. To tackle with the differentialimode noise, we add a capacitor to filter out the differentialimode noise.

With the resultant CS filter in Figure 12, which combines commonïmode and differentialïmode filters, the bandwidth of a lowpass filter for the differential CS signals becomes

$$f_{BW-diff} = \frac{1}{2 \cdot 2R_{f} \cdot C_{d} + \frac{1}{2} \cdot C_{q}} \qquad (eq. 8)$$

The bandwidth of the filter should be set based on noise that isgenerated in actual design res**lu**ta 5 kW reference design for FAN9673 with 40 kHz of switching frequency, we set $f_{BW \ common}$ at 154 kHz an $f_{BW \ diff}$ at 51.3 kHz.

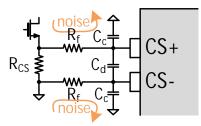


Figure 12. CS Pin Filter

Effect of Input Range Setting

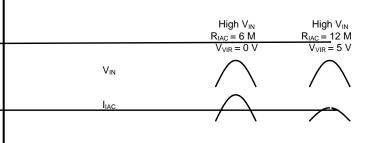
VIR pin of FAN967x sets two different modes that optimize for universal input range and European input range, respectively. This pin sources a constant current.

A resistance value connecting between VIR and GND decides the voltage on the VIR pin. The voltage on the VIR pin needs to be set higher than 3.5 V or lower than 1.5 V. Avoid anything in between.

The setting on the VIR pin changes some internal signals of FAN967x, which are collected in Table 1. M_{RLPK} constant appears in the ble. According to the test cases of V_{LPK} , which can be found in electrical characteristics in the datasheet, M_{LPK} is 2.465.

Table 1. Effects of VIR Setting

V _{VIR}	< 1.5 V	> 3.5 V
Optimized for	Universal ïinput range (90~264 Vac)	European ïinput





To make inductor track current command well, the bandwidthof the current tracking loop need to set high enough. When the complex pole formedLbgrndC_{OUT} is at a frequency much lower than the control bandwidth of $T_{I}(s)$

$$Loopgain(s) \quad \frac{(V_{\text{IN.PEAK}} |sin(t)|)^2}{V_{\text{IN.RMS}}^2} \quad \frac{1}{V_{\text{OUT}}} \quad \frac{1}{s} \quad \frac{1}{C_{\text{OUT}}} \quad \frac{P_{\text{MAX}}}{(V_{\text{VEA.MAX}} \quad 0.6)} \quad \frac{V_{\text{FBPFC}}}{V_{\text{OUT}}} \quad G_{\text{mv}}(s)$$
(eq. 25)

$$Loopgain(s)_{ac \ cycle} \quad \frac{1}{s} \quad C_{\text{OUT}} \quad (V_{\text{VEA.MAX}} \quad 0.6) \quad V_{\text{OUT}}$$