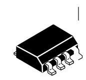
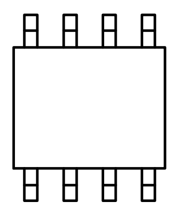
http://onsemi.com



SOIC−8
V SUFFIX
CASE 751BD

PIN CONFIGURATION



- Available in 8−pin SOIC Package
- These Devices are Pb−Free, Halogen Free/BFR Free and are RoHS Compliant

Applications

- Negative Voltage Generator
- Voltage Doubler
- Voltage Splitter
- Low EMI Power Source
- GaAs FET Biasing
- Lithium Battery Power Supply
- Instrumentation
- LCD Contrast Bias
- Cellular Phones, Pagers

July, 2012 − Rev. 12

Operation

Table 2. ABSOLUTE MAXIMUM RATINGS

Parameters	Ratings	Units
V+ to GND	6	V
Input Voltage (Pins 1, 6 and 7)	−0.3 to (V+ + 0.3)	V
BOOST/FC and OSC Input Voltage	The least negative of (Out − 0.3 V) or (V+ − 6 V) to (V+ + 0.3 V)	V
Output Short−circuit Duration to GND (OUT may be shorted to GND for 1 sec without damage but shorting OUT to V+ should be avoided.)	1	sec.
Continuous Power Dissipation (T_A = 70°C) Plastic DIP SO TDFN	 730 500 1	 mW mW W
Storage Temperature	−65 to +160	°C
Lead Soldering Temperature (10 sec)	300	°C
ESD Rating − Human Body Model	2000	V
Operating Ambient Temperature Range	−40 to +85	°C

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

NOTE: T_A = Ambient Temperature

Table 3. ELECTRICAL CHARACTERISTICS (V+ = 5 V, C1 = C2 = 100 μF, Boost/FC = Open, C_{OSC} = 0 pF, and Test Circuit is Figure 3 unless otherwise noted. Temperature is $T_A = T_{AMIN}$ to T_{AMAX} unless otherwise noted.)

Parameter	Symbol	Conditions	Min	Typ	Max	Units
Supply Voltage	VS	Inverter: LV = Open, R_L = 1 kΩ	3.0		5.5	V
		Inverter: LV = GND, R_L = 1 kΩ	1.5		5.5	
		Doubler: LV = OUT, R_L = 1 kΩ	2.5		5.5	
Supply Current	IS	BOOST/FC = open, LV = Open		0.2	0.5	mA
		BOOST/FC = V+, LV = Open		1	3	
Output Current	IOUT	OUT is more negative than −4 V	100			mA
Output Resistance	RO	C1 = C2 = 10 μF BOOST/FC = V+ (C1, C2 ESR ≤ 0.5 Ω)		3.5	10	Ω
		C1 = C2 = 100 μF (Note 5)		3.5	10	
Oscillator Frequency (Note 6)	FOSC	BOOST/FC = Open	10	25		kHz
		BOOST/FC = V+	80	135		
OSC Input Current	IOSC	BOOST/FC = Open BOOST/FC = V+		±2 ±10		μA
Power Efficiency	PE	R_L = 1 kΩ connected between V+ and OUT, T_A = 25°C (Doubler)	96	98		%
		R_L = 500 Ω connected between GND and OUT, T_A = 25°C (Inverter)	92	96		
		I_L = 100 mA to GND, T_A = 25°C (Inverter)		88		
Voltage Conversion Efficiency	VEFF	No load, T_A = 25°C	99	99.9		%

4. In Figure 3, test circuit electrolytic capacitors C1 and C2 are 100 μF and have 0.2 Ω maximum ESR. Higher ESR levels may reduce efficiency and output voltage.
5. The output resistance is a combination of the internal switch resistance and the external capacitor ESR. For maximum voltage and efficiency keep external capacitor ESR under 0.2 Ω.
6. FOSC is tested with C_{OSC} = 100 pF to minimize test fixture loading. The test is correlated back to C_{OSC} = 0 pF to simulate the capacitance at OSC when the device is inserted into a test socket without an external C_{OSC}.

Voltage Inverter

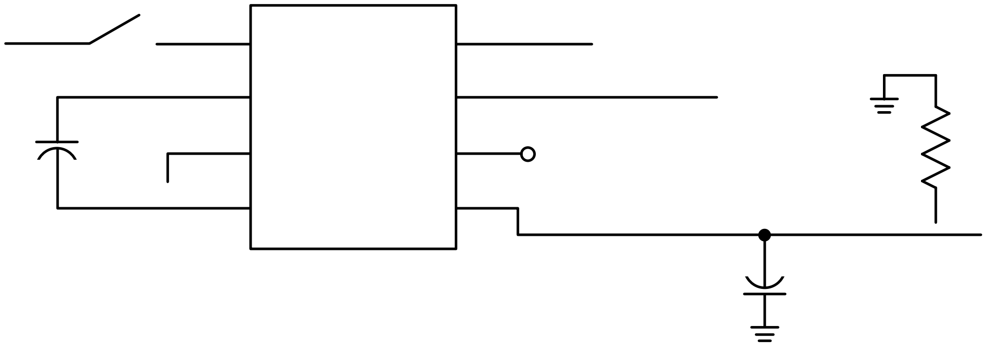


Figure 3. Test Circuit Voltage Inverter

TYPICAL OPERATING CHARACTERISTICS

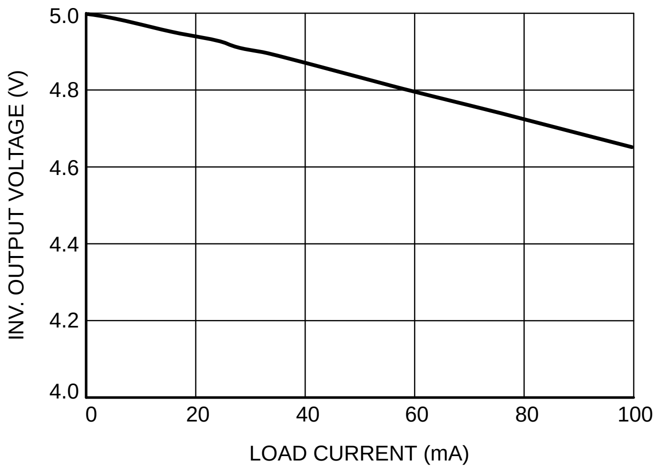


Figure 8. Inverted Output Voltage vs. Load, V+ = 5 V

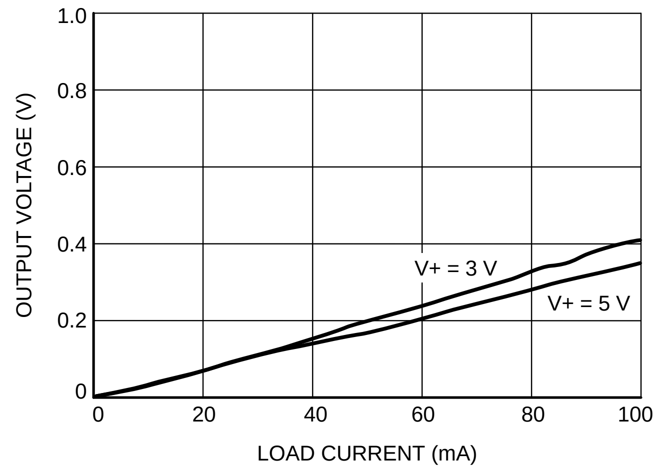


Figure 9. Output Voltage Drop vs. Load Current

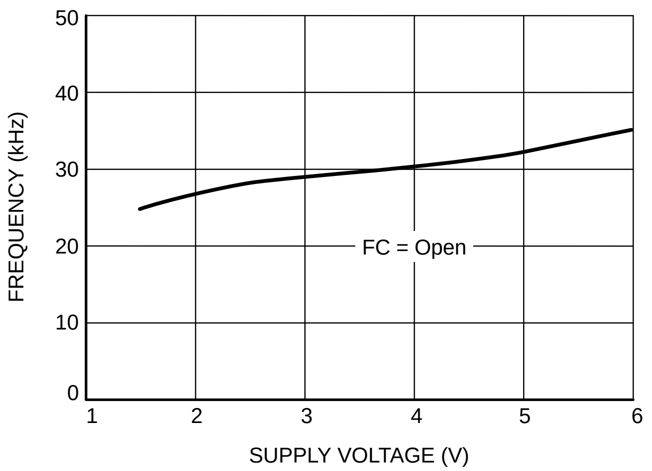


Figure 10. Oscillator Frequency vs. Supply Voltage

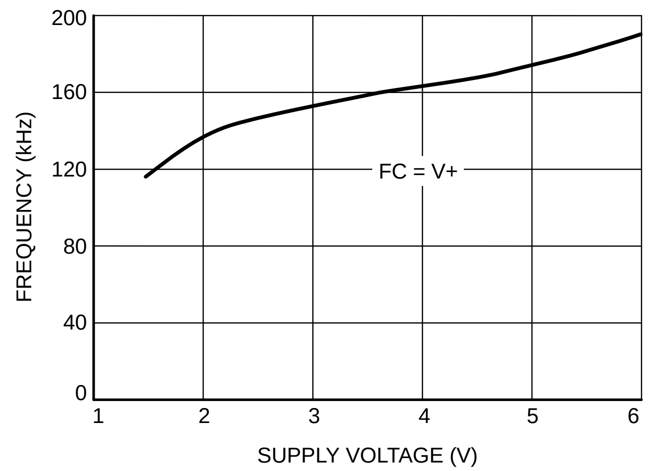


Figure 11. Oscillator Frequency vs. Supply Voltage

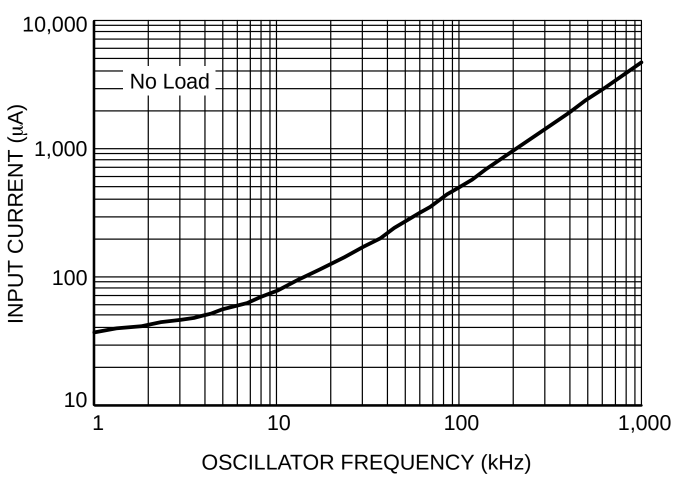


Figure 12. Supply Current vs. Oscillator Frequency

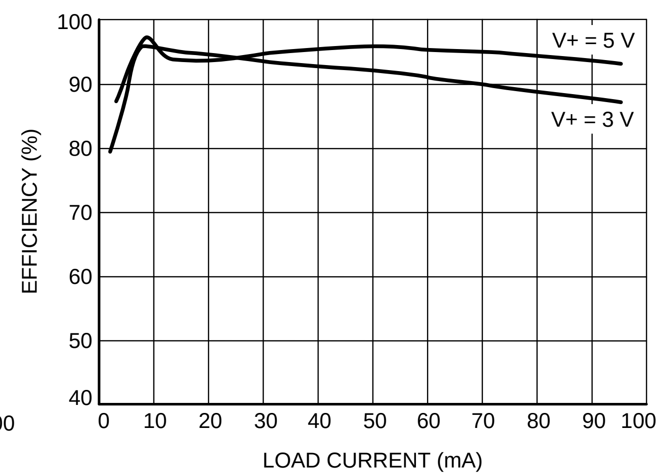


Figure 13. Efficiency vs. Load Current

Voltage Doubler

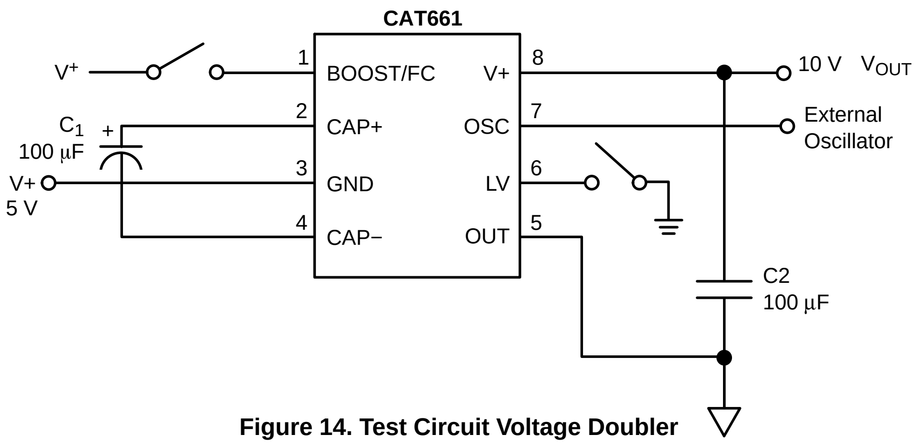


Figure 14. Test Circuit Voltage Doubler

TYPICAL OPERATING CHARACTERISTICS

(Typical characteristic curves are generated using the circuit in Figure 14. Doubler test conditions are: V+ = 5 V, LV = GND, BOOST/FC = Open and T_A = 25°C unless otherwise indicated.)

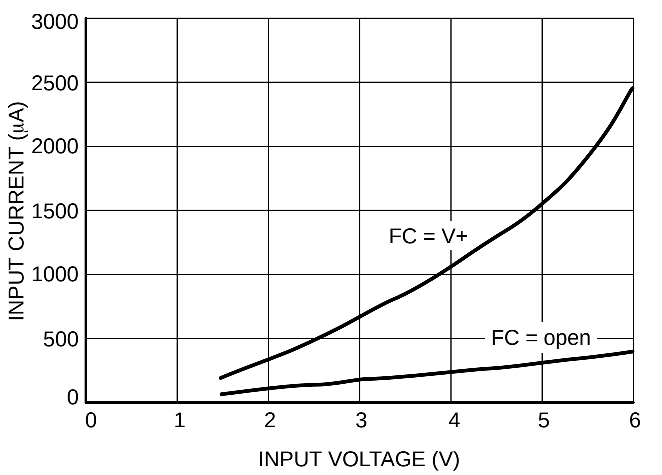


Figure 15. Supply Current vs. Input Voltage (No Load)

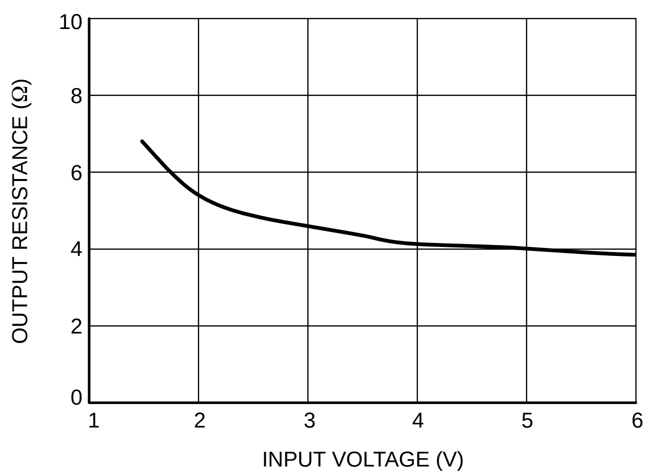


Figure 16. Output Resistance vs. Input Voltage

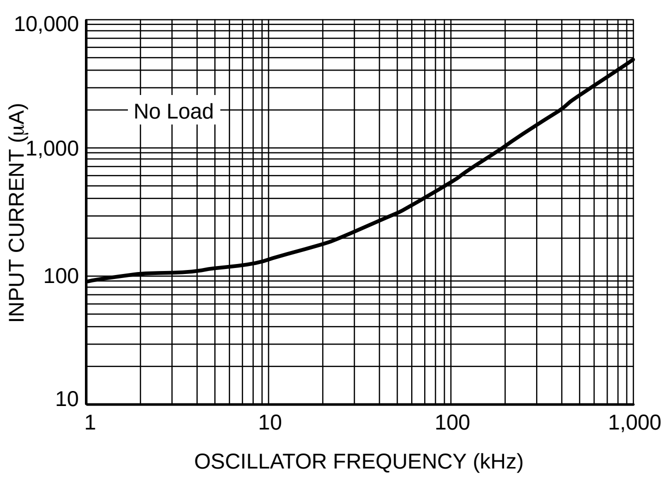


Figure 17. Supply Current vs. Oscillator Frequency

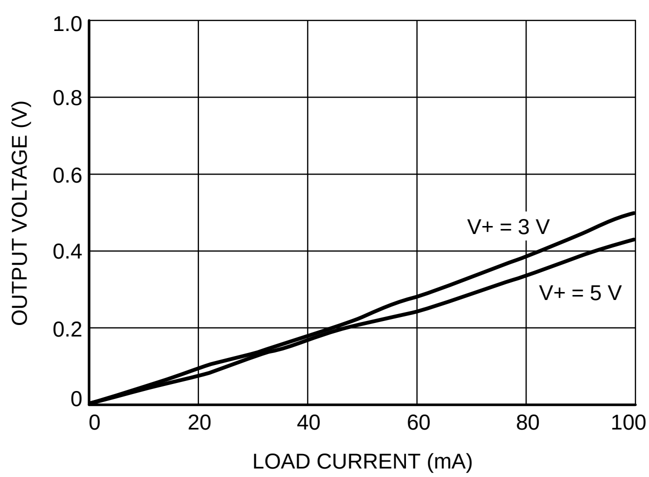


Figure 18. Output Voltage Drop vs. Load Current

Application Information

Circuit Description and Operating Theory

The CAT661 switches capacitors to invert or double an input voltage.

Figure 19 shows a simple switch capacitor circuit. In position 1 capacitor C1 is charged to voltage V1. The total charge on C1 is Q1 = C1V1. When the switch moves to position 2, the input capacitor C1 is discharged to voltage V2. After discharge, the charge on C1 is Q2 = C1V2.

The charge transferred is:

$$\Delta Q = Q1 - Q2 = C1 \times (V1 - V2)$$

If the switch is cycled "F" times per second, the current (charge transfer per unit time) is:

$$I = F \times \Delta Q = F \times C1\,(V1 - V2)$$

Rearranging in terms of impedance:

$$I = \frac{(V1 - V2)}{(1/FC1)} = \frac{V1 - V2}{REQ}$$

The 1/FC1 term can be modeled as an equivalent impedance REQ. A simple equivalent circuit is shown in Figure 20. This circuit does not include the switch resistance nor does it include output voltage ripple. It does allow one to understand the switch−capacitor topology and make prudent engineering tradeoffs.

For example, power conversion efficiency is set bjET0 G..0001 2d as

The 1/F, willpleminat inclunclude 5 Tw[im, as 8588usngie total)]TT*

Oscillator Frequency Control

The switching frequency can be raised, lowered or driven from an external source. Figure 22 shows a functional diagram of the oscillator circuit.

The CAT661 oscillator has four control modes:

Table 4.

BOOST/FC Pin Connection

Capacitor Selection

Low ESR capacitors are necessary to minimize voltage losses, especially at high load currents. The exact values of C1 and C2 are not critical but low ESR capacitors are necessary.

The ESR of capacitor C1, the pump capacitor, can have a pronounced effect on the output. C1 currents are approximately twice the output current and losses occur on both the charge and discharge cycle. The ESR effects are thus multiplied by four. A 0.5 Ω ESR for C1 will have the same effect as a 2 Ω increase in CAT661 output impedance.

Output voltage ripple is determined by the value of C2 and the load current. C2 is charged and discharged at a current roughly equal to the load current. The internal switching frequency is one−half the oscillator frequency.

$$VRIPPLE = IOUT/(FOSC \times C2) + IOUT \times ESRC2$$

For example, with a 25 kHz oscillator frequency (12.5 kHz switching frequency), a 150 μF C2 capacitor with an ESR of 0.2 Ω and a 100 mA load peak−to−peak ripple voltage is 45 mV.

Table 5. VRIPPLE vs. FOSC

VRIPPLE (mV)	IOUT (mA)	FOSC (kHz)	C2 (μF)	C2 ESR (Ω)
45	100	25		

Capacitor Suppliers

The following manufacturers supply low−ESR capacitors:

Table 6. CAPACITOR SUPPLIERS

Manufacturer	Capacitor Type	Phone	WEB	Email	Comments
AVX/Kyocera	TPS/TPS3	843−448−9411	www.avxcorp.com	avx@avxcorp.com	Tantalum
Vishay/Sprague	595	402−563−6866	www.vishay.com	−	Aluminum
Sanyo	MV−AX, UGX	619−661−6835	www.sanyo.com	Svcsales@sanyo.com	Aluminum
Nichicon	F55	847−843−7500	www.nichicon−us.com	−	Tantalum
	HC/HD				Aluminum

Capacitor manufacturers continually introduce new series and offer different package styles. It is recommended that before a design is finalized capacitor manufacturers should be surveyed for their latest product offerings.

Controlling Loss in CAT661 Applications

There are three primary sources of voltage loss:

1. Output resistance:
   VLOSS = ILOAD x ROUT, where ROUT is the CAT661 output resistance and ILOAD is the load current.
2. Charge pump (C1) capacitor ESR:
   VLOSSC1 ≈ 4 x ESRC1 x ILOAD, where ESRC1 is the ESR of capacitor C1.
3. Output or reservoir (C2) capacitor ESR:
   VLOSSC2 = ESRC2 x ILOAD, where ESRC2 is the ESR of capacitor C2.

Increasing the value of C2 and/or decreasing its ESR will reduce noise and ripple.

The effective output impedance of a CAT661 circuit is approximately:

$$R_{circuit} \approx R_{out\,661} + (4 \times ESR_{C1}) + ESR_{C2}$$

Typical Applications

Voltage Inversion Positive–to–Negative

Precision Voltage Divider

A precision voltage divider is shown in Figure 26. With load currents under 100 nA, the voltage at pin 2 will be within 0.002% of V+/2.

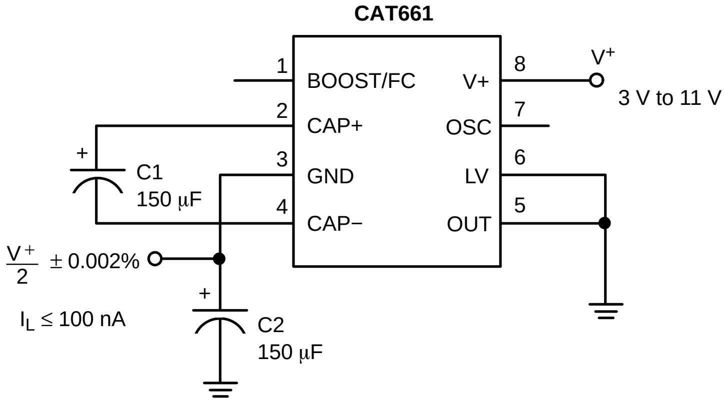


Figure 26. Precision Voltage Divider (Load ≤ 100 nA)

Battery Voltage Splitter

Positive and negative voltages that track each other can be obtained from a battery. Figure 27 shows how a 9 V battery can provide symmetrical positive and negative voltages equal to one−half the battery voltage.

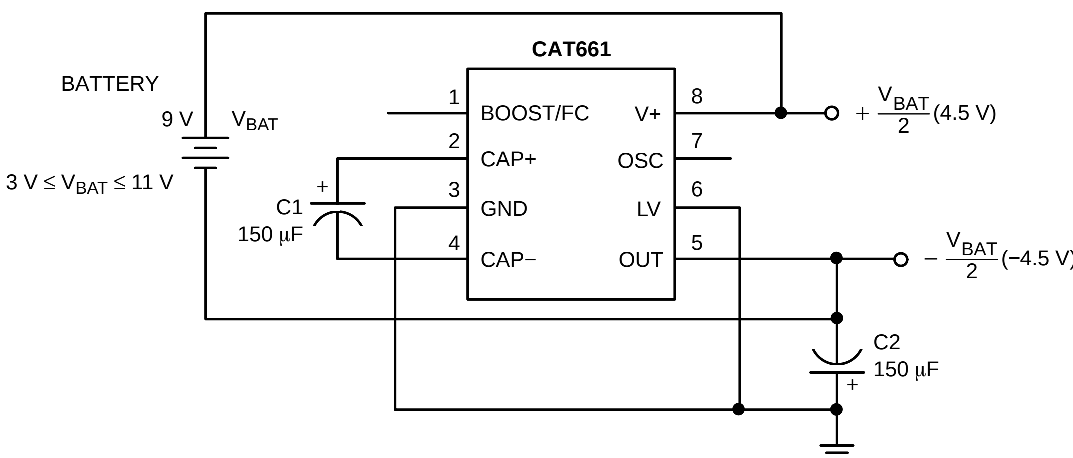


Figure 27. Battery Splitter

Cascade Operation for Higher Negative Voltages

The CAT661 can be cascaded as shown in Figure 28 to generate more negative voltage levels. The output resistance is approximately the sum of the individual CAT661 output resistance.

$V_{OUT} = -N \times V_{IN}$, where N represents the number of cascaded devices.

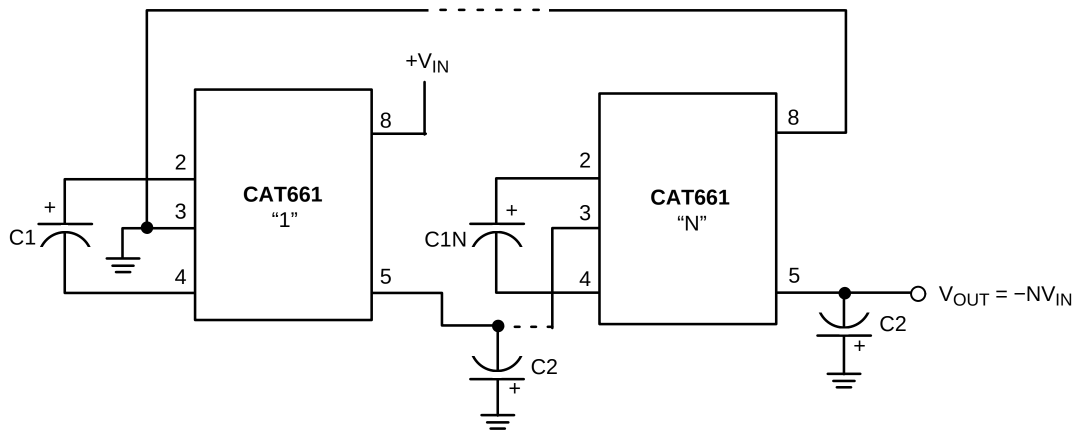


Figure 28. Cascading to Increase Output Voltage

Parallel Operation